

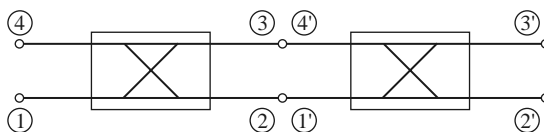
- [17] D. W. Kammler, "The Design of Discrete  $N$ -Section and Continuously Tapered Symmetrical TEM Directional Couplers," *IEEE Transactions on Microwave Theory and Techniques*, vol. MTT-17, pp. 577–590, August 1969.

## PROBLEMS

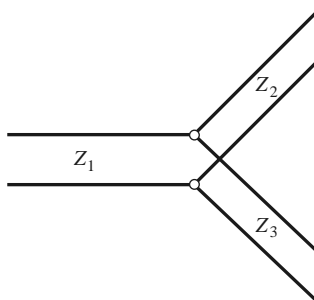
- 7.1 Write the scattering matrix for a nonideal symmetric hybrid coupler in terms of the coupler parameters,  $C$ ,  $D$ ,  $I$ , and  $L$ , as defined in (7.20). Repeat for a nonideal antisymmetric hybrid coupler. Assume that the couplers are matched at all ports.
- 7.2 A 20 dBm power source is connected to the input of a directional coupler having a coupling factor of 20 dB, a directivity of 35 dB, and an insertion loss of 0.5 dB. If all ports are matched, find the output powers (in dBm) at the through, coupled, and isolated ports.
- 7.3 A directional coupler has the scattering matrix given below. Find the return loss, coupling factor, directivity, and insertion loss. Assume that the ports are terminated in matched loads.

$$[S] = \begin{bmatrix} 0.1\angle 40^\circ & 0.944\angle 90^\circ & 0.178\angle 180^\circ & 0.0056\angle 90^\circ \\ 0.944\angle 90^\circ & 0.1\angle 40^\circ & 0.0056\angle 90^\circ & 0.178\angle 180^\circ \\ 0.178\angle 180^\circ & 0.0056\angle 90^\circ & 0.1\angle 40^\circ & 0.944\angle 90^\circ \\ 0.0056\angle 90^\circ & 0.178\angle 180^\circ & 0.944\angle 90^\circ & 0.1\angle 40^\circ \end{bmatrix}$$

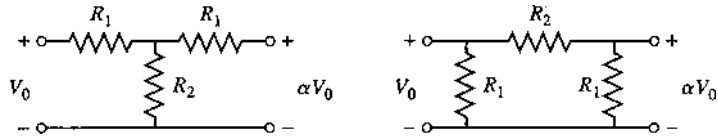
- 7.4 Two identical  $90^\circ$  couplers with  $C = 8.34$  dB are connected as shown below. Find the resulting phase and amplitudes at ports 2' and 3', relative to port 1.



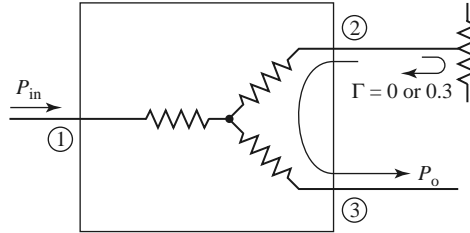
- 7.5 Consider the T-junction of three lines with characteristic impedances  $Z_1$ ,  $Z_2$ , and  $Z_3$ , as shown below. Demonstrate that it is impossible for all three lines to be matched when looking toward the junction.



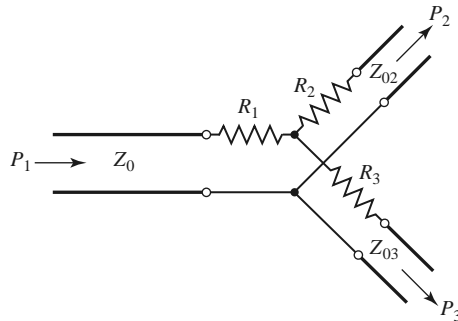
- 7.6 Design a lossless T-junction divider with a  $30\ \Omega$  source impedance to give a 3:1 power split. Design quarter-wave matching transformers to convert the impedances of the output lines to  $30\ \Omega$ . Determine the magnitude of the scattering parameters for this circuit, using a  $30\ \Omega$  characteristic impedance.
- 7.7 Consider the T and  $\pi$  resistive attenuator circuits shown below. If the input and output are matched to  $Z_0$ , and the ratio of output voltage to input voltage is  $\alpha$ , derive the design equations for  $R_1$  and  $R_2$  for each circuit. If  $Z_0 = 50\ \Omega$ , compute  $R_1$  and  $R_2$  for 3, 10, and 20 dB attenuators of each type.



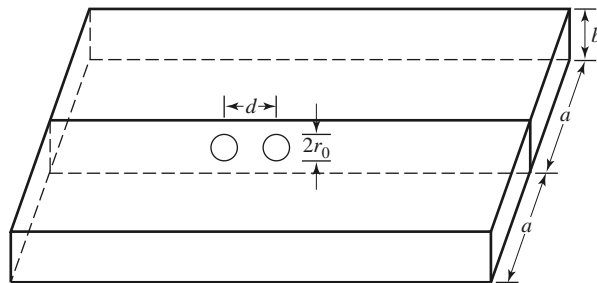
- 7.8 Design a three-port resistive divider for an equal power split and a  $100\ \Omega$  system impedance. If port 3 is matched, calculate the change in output power at port 3 (in dB) when port 2 is connected first to a matched load, and then to a load having a mismatch of  $\Gamma = 0.3$ . See the figure below.



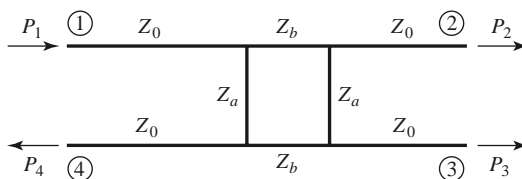
- 7.9 Consider the general resistive divider shown below. For an arbitrary power division ratio  $\alpha = P_2/P_3$ , derive expressions for the resistors  $R_1$ ,  $R_2$ , and  $R_3$ , and the output characteristic impedances  $Z_{o2}$  and  $Z_{o3}$  so that all ports are matched, assuming the source impedance is  $Z_0$ .



- 7.10 Design a Wilkinson power divider with a power division ratio of  $P_3/P_2 = 1/3$  and a source impedance of  $50\ \Omega$ .
- 7.11 Derive the design equations in (7.37a)–(7.37c) for the unequal-split Wilkinson divider.
- 7.12 For the Bethe hole coupler of the type shown in Figure 7.16a, derive a design for  $s$  so that port 3 is the isolated port.
- 7.13 Design a Bethe hole coupler of the type shown in Figure 7.16a for a Ku-band waveguide operating at 11 GHz. The required coupling is 20 dB.
- 7.14 Design a Bethe hole coupler of the type shown in Figure 7.16b for a Ku-band waveguide operating at 17 GHz. The required coupling is 30 dB.
- 7.15 Design a five-hole directional coupler in a Ku-band waveguide with a binomial directivity response. The center frequency is 17.5 GHz, and the required coupling is 20 dB. Use round apertures centered across the broad wall of the waveguides.
- 7.16 Repeat Problem 7.14 for a design with a Chebyshev response, having a minimum directivity of 30 dB.
- 7.17 Develop the necessary equations required to design a two-hole directional coupler using two waveguides with apertures in a common sidewall, as shown below.

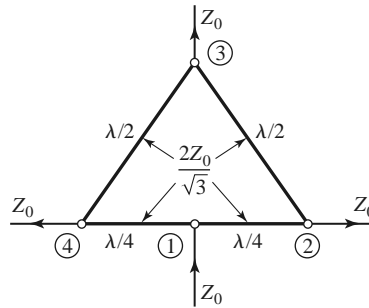


- 7.18** Consider the general branch-line coupler shown below, with shunt arm characteristic impedances  $Z_a$  and series arm characteristic impedances  $Z_b$ . Using an even-odd mode analysis, derive design equations for a quadrature hybrid coupler with an arbitrary power division ratio of  $\alpha = P_2/P_3$ , and with the input port (port 1) matched. Assume all arms are  $\lambda/4$  long. Is port 4 isolated, in general?

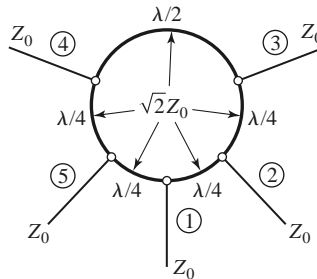


- 7.19** An edge-coupled stripline with a ground plane spacing of 2.0 mm and a dielectric constant of 4.2 has strip widths of 0.6 mm and a separation of 0.2 mm between the edges of the strips. Use the graph of Figure 7.29 to find the resulting even- and odd-mode characteristic impedances. If possible, compare your results to those obtained from a microwave CAD tool.
- 7.20** A coupled microstrip line is to be designed for a substrate having a thickness of 2.0 mm and dielectric constant of 10.0. The required even- and odd-mode characteristic impedances are 133  $\Omega$  and 71.5  $\Omega$ , respectively. Use the graph of Figure 7.30 to find the required line widths and separation. If possible, compare your results to those obtained from a microwave CAD tool.
- 7.21** Repeat the derivation in Section 7.6 for the design equations of a single-section coupled line coupler using reflection and transmission coefficients instead of voltages and currents.
- 7.22** Design a single-section coupled line coupler with a coupling of 19.1 dB, a system impedance of 60  $\Omega$ , and a center frequency of 8 GHz. If the coupler is to be made in stripline (edge-coupled), with  $\epsilon_r = 2.2$  and  $b = 0.32$  cm, find the necessary strip widths and separation.
- 7.23** Repeat Problem 7.22 for a coupling factor of 5 dB. Is this a practical design?
- 7.24** Derive Equations (7.83) and (7.84).
- 7.25** A 20-dB three-section coupled line coupler is required to have a maximally flat coupling response with a center frequency of 3 GHz and  $Z_0 = 50 \Omega$ . (a) Design the coupler and find  $Z_{0e}$  and  $Z_{0o}$  for each section. Use CAD to plot the resulting coupling (in dB) from 1 to 5 GHz. (b) Lay out the microstrip implementation of the coupler on an FR4 substrate having  $\epsilon_r = 4.2$ ,  $d = 0.158$  cm, and  $\tan \delta = 0.02$ , with copper conductors 0.5 mil thick. Use CAD to plot the insertion loss versus frequency.
- 7.26** Repeat Problem 7.25 for a coupler with an equal-ripple coupling response, where the ripple in the coupling is 1 dB over the passband.
- 7.27** For the Lange coupler, derive the design equations (7.100) for  $Z_{0e}$  and  $Z_{0o}$  from (7.98) and (7.99).
- 7.28** Design a 3 dB Lange coupler for operation at 5 GHz. If the coupler is to be fabricated in microstrip on an alumina substrate with  $\epsilon_r = 10$  and  $d = 1.0$  mm, compute  $Z_{0e}$  and  $Z_{0o}$  for the two adjacent lines, and find the necessary spacing and widths of the lines.
- 7.29** An input signal  $V_1$  is applied to the sum port of a  $180^\circ$  hybrid, and another signal  $V_4$  is applied to the difference port. What are the output signals?

- 7.30** Calculate the even- and odd-mode characteristic impedances for a tapered coupled line  $180^\circ$  hybrid coupler with a 3 dB coupling ratio and a  $50\ \Omega$  characteristic impedance.
- 7.31** Find the scattering parameters for the four-port Bagley polygon power divider shown below.



- 7.32** For the symmetric hybrid shown below, calculate the output voltages if port 1 is fed with an incident wave of  $1\angle 0$  V. Assume that the outputs are matched.



- 7.33** The Bailey unequal-split power divider uses a  $90^\circ$  hybrid coupler and a T-junction, as shown below. The power division ratio is controlled by adjusting the feed position,  $a$ , along the transmission line of length  $b$  that connects ports 1 and 4 of the hybrid. A quarter-wave transformer of impedance  $Z_0/\sqrt{2}$  is used to match the input of the divider. (a) For  $b = \lambda/4$ , show that the output power division ratio is given by  $P_3/P_2 = \tan^2(\pi a/2b)$ . (b) Using a branch-line hybrid with  $Z_0 = 50\ \Omega$ , design a power divider with a division ratio of  $P_3/P_2 = 0.5$ , and plot the resulting input return loss and transmission coefficients versus frequency.

